



THE UNIVERSITY OF  
**NEWCASTLE**  
AUSTRALIA



**SCHULICH**  
School of Engineering



## **Designing an Easily-Made Lattice Tower for a Small Wind Turbine**

P.D. Clausen<sup>1</sup>, P. Peterson<sup>2</sup>, S.V.R. Wilson<sup>2</sup>, D.H.  
Wood<sup>2,3</sup>

<sup>1</sup>School of Engineering, University of Newcastle,  
NSW 2308, Australia

<sup>2</sup>Aerogenesis Australia, PO Box 153, Shortland Bldg,  
NSW 2308, Australia

<sup>3</sup>Dept Mechanical & Manufacturing Eng'g, University  
of Calgary, Calgary T2N 1N4, Canada



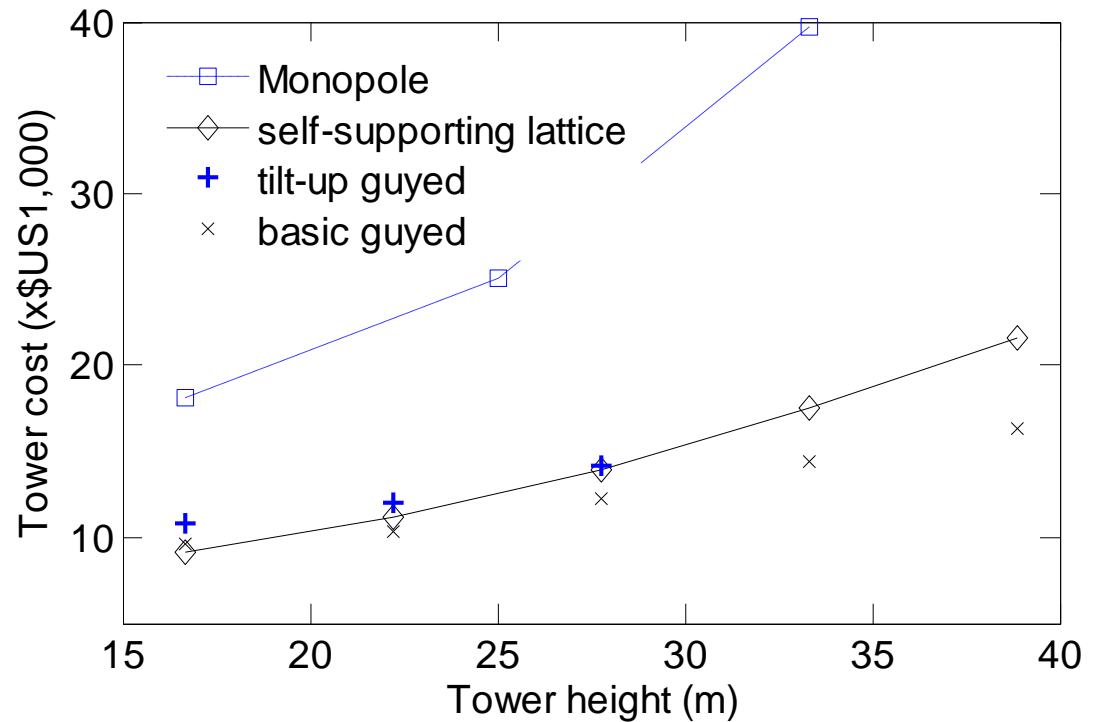
THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA



SCHULICH  
School of Engineering



## Monopole towers are becoming common but are expensive



USD price for towers for the Bergey 10 kW turbine



THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA



SCHULICH  
School of Engineering



Connection  
plates  
ignored in  
initial  
analysis



Lattice towers are easily made as in this  
jig at Kijito Windpower Kenya



THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA



SCHULICH  
School of Engineering



## Aim: to design an easily-made lattice tower for the Aerogenesis 5 kW wind turbine

Design wind speed	52.5 m/s (IEC Class III)
General specifications for turbine	Height:18 m Turbine mass: 170 kg Maximum thrust: 2.2 kN. Two blades with maximum speed 320 rpm
General specifications for tower for compatibility with existing towers	Base distance between legs :1.975 m Length of tower sections: 2.98 m
Vertical and horizontal members	Low carbon steel: $F_y = 255$ MPa. 60.5mm diameter pipe. Wall thickness: 3.65mm
Cross Bracing	Low carbon steel: $F_y = 255$ MPa Solid round bar, 12.7 mm diameter

Same materials as for windmill towers



THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA



SCHULICH  
School of Engineering



*“In the analysis of towers the largest uncertainty is an accurate knowledge of the wind loads. Highly sophisticated methods of analysis cannot improve this. A linear-static three-dimensional structural analysis is sufficient for almost all lattice tower structures”, Steel Designers Manual. Davison B, Owens GW (eds) The Steel Construction Institute, Blackwell Science, 2003.*

**Need finite element linear static analysis (FEA) for a range of wind directions**



THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA

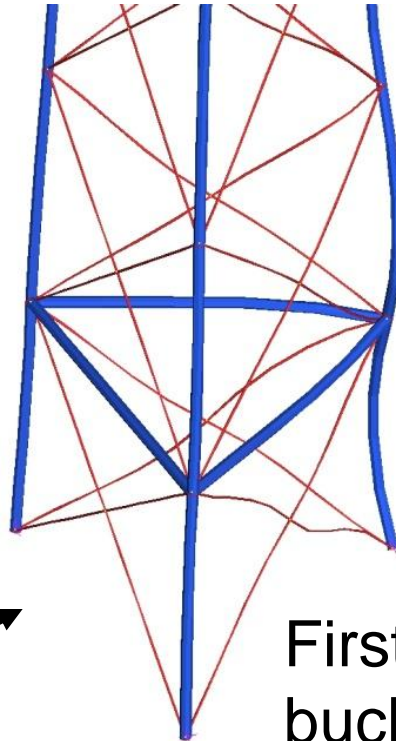
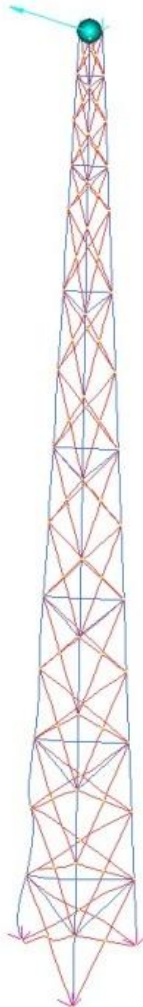


SCHULICH  
School of Engineering



## Finite Element Analysis

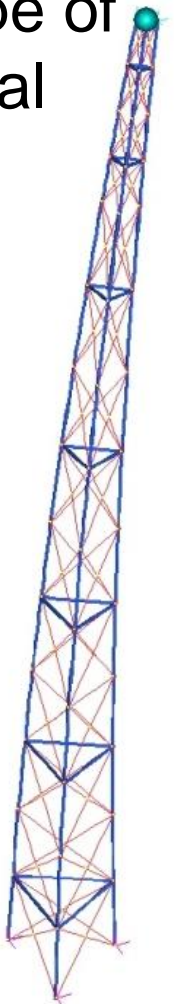
turbine



Wind  
direction

First  
buckling  
mode

Mode shape of  
fundamental  
frequency



FE Model



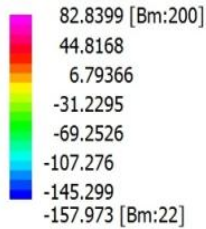
THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA



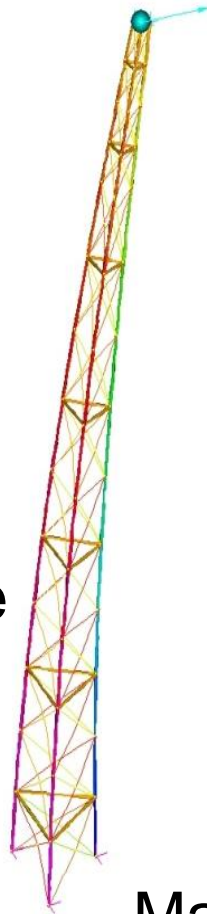
SCHULICH  
School of Engineering



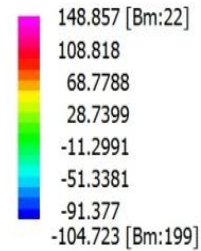
Fibre Stress (MPa)



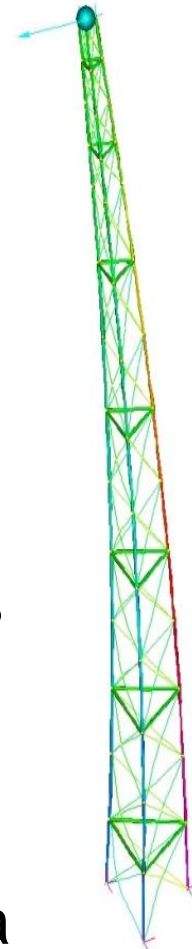
Maximum  
compressive  
stress = 158  
MPa



Fibre Stress (MPa)



Maximum  
tensile stress  
= 149 MPa



Material yield stress = 255 MPa



THE UNIVERSITY OF  
NEWCASTLE  
AUSTRALIA



SCHULICH  
School of Engineering



## Buckling Calculations

Factor = load required for buckling / (maximum actual load)

1. Linear buckling factor from FEA = 4
2. ASCE (1990) guidelines factor  $\approx 2$
3. Eurocode 3 factor  $\approx 2$

The last two are empirical and so take some account of manufacturing defects





THE UNIVERSITY OF  
**NEWCASTLE**  
AUSTRALIA



**SCHULICH**  
School of Engineering



<b>Parameter</b>	<b>Monopole Tower</b>	<b>Lattice Tower</b>
Mass (kg)	861	640
Natural Frequency (Hz)	0.84	2.53
Maximum blade passing frequency (1P) Hz	5.3	5.3
Turbine deflection at 52.5 m/s (m)	0.73	0.32



THE UNIVERSITY OF  
**NEWCASTLE**  
AUSTRALIA



**SCHULICH**  
School of Engineering



## Conclusions

1. A lattice tower was designed to be built easily using existing facilities and materials for a two-bladed 5 kW wind turbine
2. Maximum tower stress = 158 MPa. Material yield stress = 255 MPa. Tower is safe
3. Tower is safe from buckling
4. Tower is lighter and stiffer, and has higher natural frequency than monopole tower



THE UNIVERSITY OF  
**NEWCASTLE**  
AUSTRALIA



**SCHULICH**  
School of Engineering

